



# SCHOOL OF ENGINEERING

TAYLOR'S UNIVERSITY

MEC60303

Theory of Machines & Mechanism

Title: Theory of Machines & Mechanism Assignment

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## 1.0 Assignment Task 1

### 1.1 Performance Ability

#### 1.1.1 Climb-Ability

Gradeability defines as a maximum gradient a vehicle can climb while sustaining a specific speed set by the driver [1].

Traction force defines as the driving force as a result of friction between the tyre and road that moves the vehicle forward [2].

For the vehicle to climb up a slope, the traction force must be greater than the resistance forces. The table 1.0 below has listed all the gears which can overcome the total resistance based on the traction force accordingly. The table below also shows that Gear A uses more gears starting from 5% gradient compared to Gear B.

Table 1.0 Tabulated Data

Resistance, %	Traction Force A, N					Traction Force B, N				
	Gear A					Gear B				
	1	2	3	4	5	1	2	3	4	5
0	√	√	√	√	√	√	√	√	√	√
3	√	√	√	√	√	√	√	√	√	√
5	√	√	√	√	√	√	√	√	√	
10	√	√	√	√		√	√	√		
15	√	√	√			√	√			
20	√	√				√				
26	√	√				√				
30	√					√				
35	√					√				

## Climb Ability

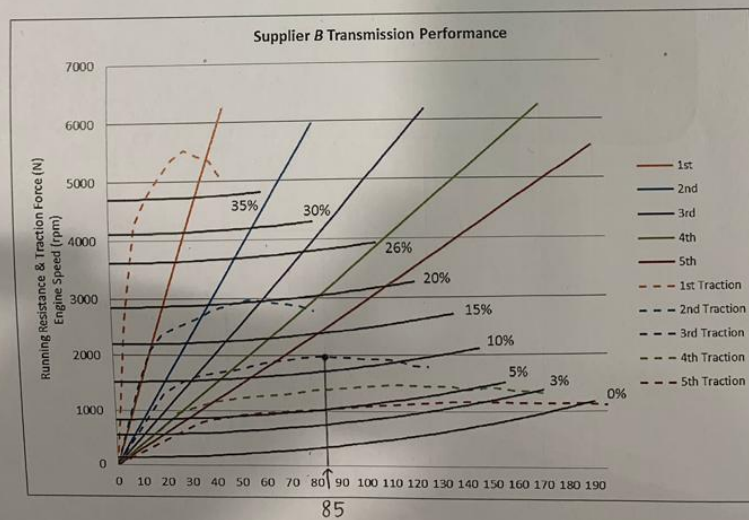
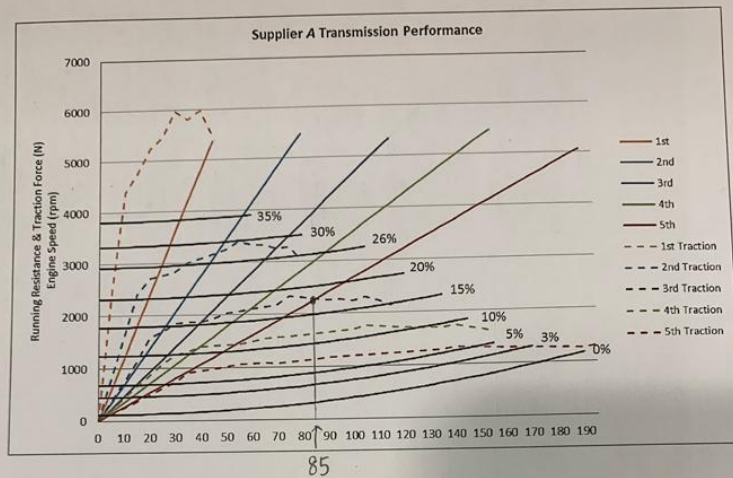


Figure 1.0 Traction Force at vehicle speed of 85 km/h

Taking a speed of 85 km/h, the transmission A can overcome a total resistance of 15% while the transmission B can only overcome a total resistance of 10% as shown in the figure above. Therefore, transmission B must lower down to gear 2 in order to overcome a total resistance of 15%. This also means that lower gear requires a greater torque as the gear size is bigger. This was proven in the torque formula:

$$\tau = F \times d$$

where  $d$  = length of arm

$F$  = force acting on direction of rotation

Also, since the torque required by transmission B is higher, a greater power will be generated to climb the gradient. In this case, transmission A possesses a better climb-ability compared to transmission B.

### 1.1.2 Response (Low Vehicle Speed)

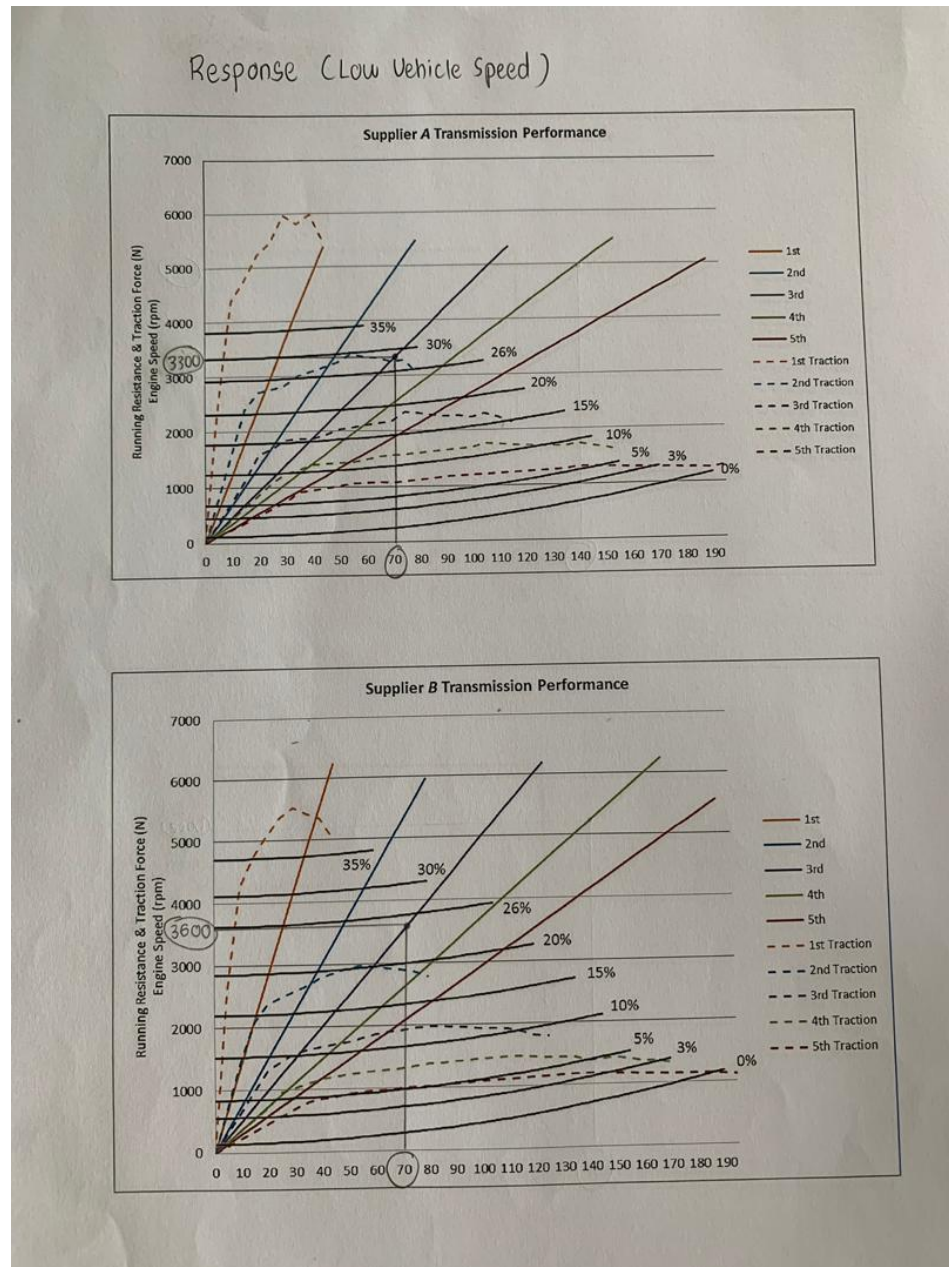


Figure 2.0 Engine Speed (rpm) at vehicle speed of 70 km/h on 3<sup>rd</sup> gear

Taking a speed of 70 km/h which lies on the 3<sup>rd</sup> gear as shown in figure 2.0 above, transmission A produces an engine speed of 3000 rpm while transmission B produces an engine speed of 3600 rpm. Therefore, transmission A has a better response at a

low vehicle speed as it has a lower engine speed (rpm) comparing to B. Lower engine speed (rpm) also means better acceleration where the vehicle can reach a higher speed in a given specified time.

Besides, transmission B has a greater coloured solid line (engine speed) gradient compared to transmission A. Hence, this also proves that transmission A gives a better response at a low vehicle speed than B as the gradient A is lower which means the engine speed is lower.

### 1.1.3 Response (High Vehicle Speed)

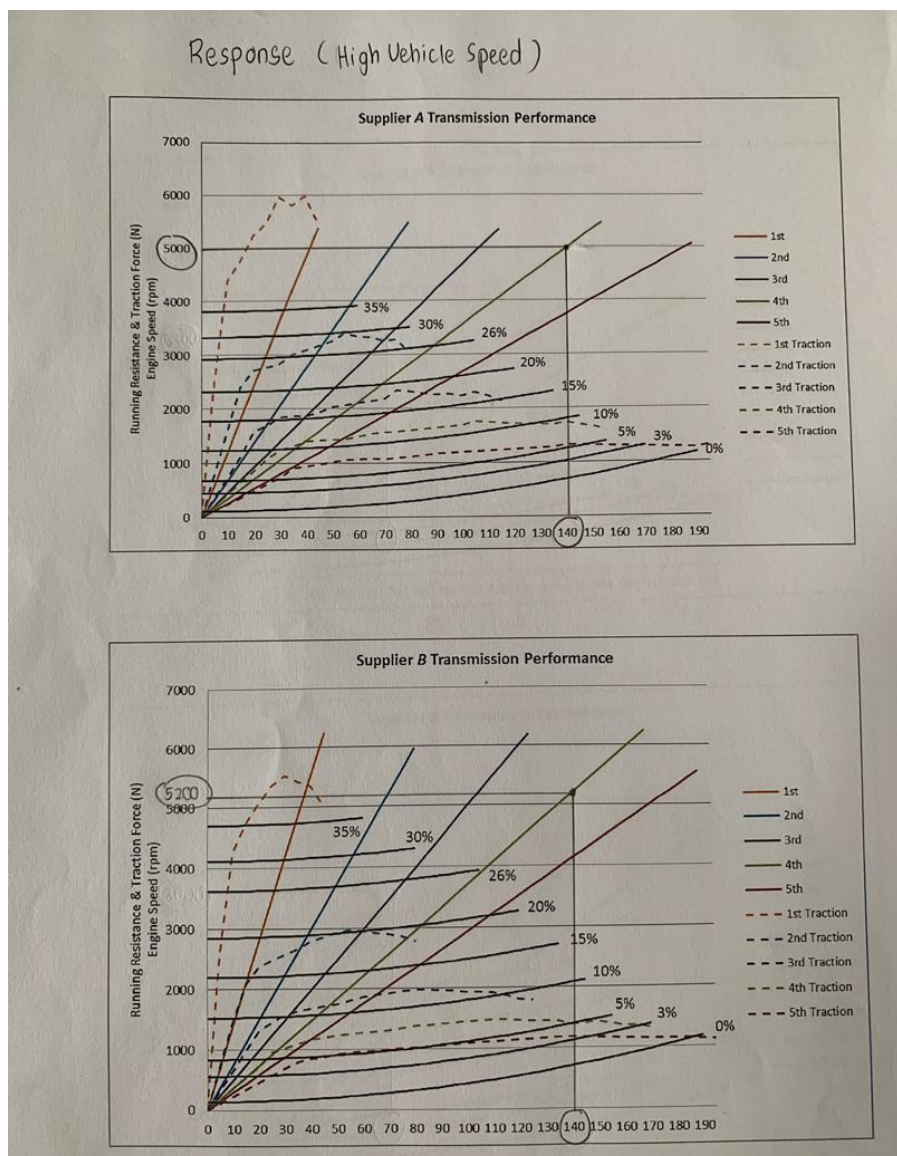


Figure 3.0 Engine Speed (rpm) at vehicle speed of 140 km/h on 4<sup>th</sup> gear



Taking a speed of 140 km/h which lies on the 4<sup>th</sup> gear as shown in figure 3.0 above, transmission A produces an engine speed of 5000 rpm while transmission B produces an engine speed of 5200 rpm. Therefore, transmission A has a better response at a high vehicle speed as it has a lower engine speed (rpm) comparing to B.

#### 1.1.4 Fuel Consumption

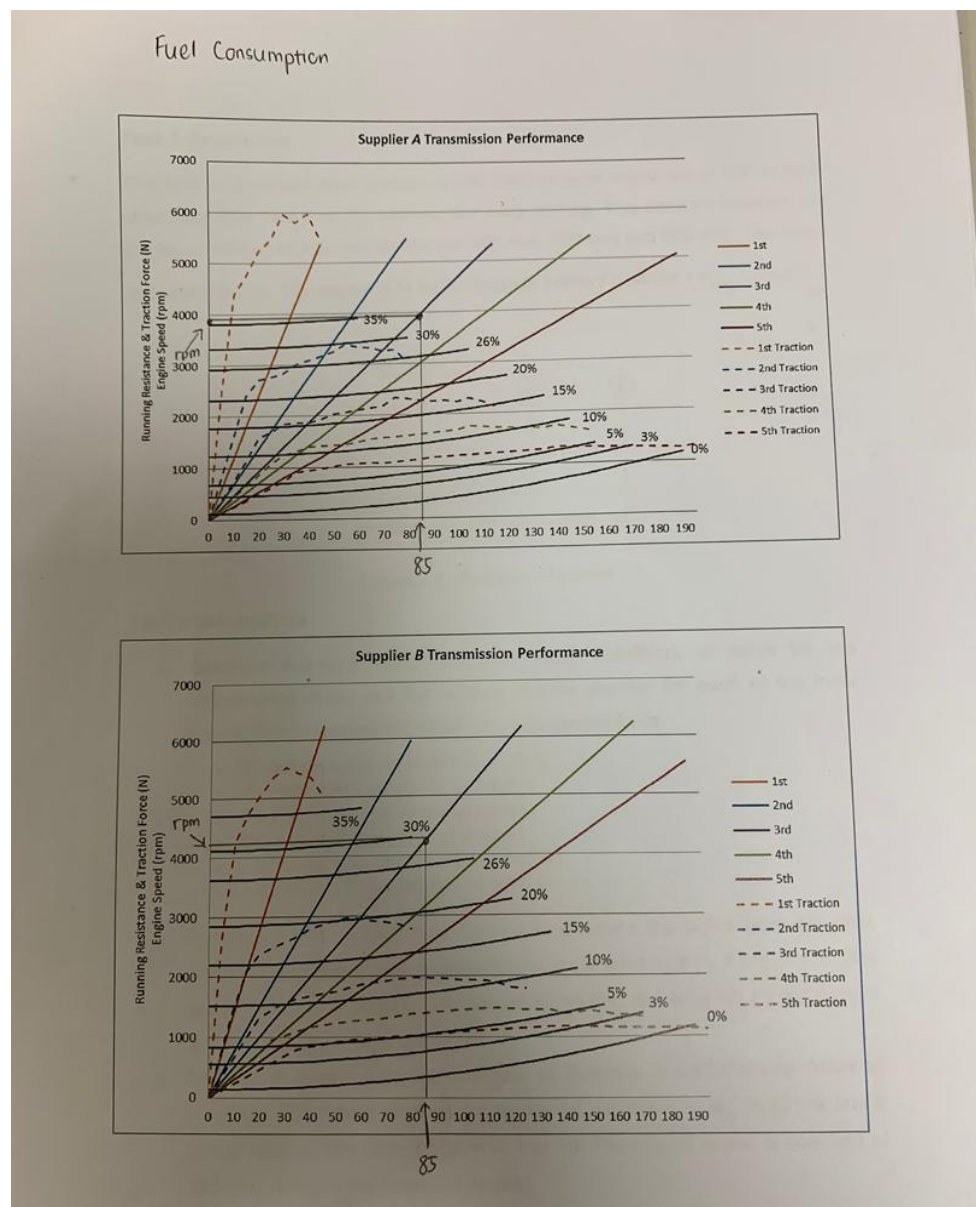


Figure 4.0 Engine Speed (rpm) at vehicle speed of 85 km/h on 3<sup>rd</sup> gear

Taking the speed of 85 km/h with a 3<sup>rd</sup> gear ratio as shown in figure 4.0 above, the transmission A indicates an estimated of 3900 rpm while the transmission B shows an estimated rpm of 4200 as shown in the figure above. A greater engine speed (rpm) requires more fuel to perform. Therefore, the fuel consumption for transmission B is greater compared to A due to its higher engine speed (rpm). In this case, transmission A gives out a better fuel consumption compared to B.

Furthermore, this can also relate to climb ability where transmission B must lower down to gear 2 in order to overcome a total resistance of 15% whereas transmission A can maintain at gear 3. This means that the consumption of fuel for transmission B is required as lower gear gives out a higher rpm. This also proves that transmission A has a better fuel consumption.

Besides that, relating to the response, transmission A has a better response at low and high vehicle speed compared to B. This shows that lesser fuel will be consumed by transmission A since it doesn't require a higher rpm to accelerate the car to a specified speed in a given time.

## 1.2 Regulation (emission requirement)

Based on the research, the pollutants emitted from the emission were nitrogen oxide, carbon monoxide, hydrocarbon, etc. Based on the data taken from the real driving emission (RDE), Euro 5 has the best RDE as it released the least pollutants compared to Euro 3 [3].

According to the emission standards which were published by the European commission, Euro 5 has a lower emission limit compared to Euro 3 [4]. This means that lesser pollutants will be released to the atmosphere by Euro 5 fuel.



In this case, transmission B is better in terms of emission compared to transmission A if environment factor is taken into consideration.

### 1.3 After Market Value

Table 2.0 Data's from both suppliers

	Supplier A Transmission	Supplier B Transmission
Warranty	60000km or 5 years	30000km or 3 years
Transmission oil service	60000km or 120000km	
Transmission oil price	RM48 per litre	RM30 per litre

According to table 2.0 above, the warranty period based on the distance for supplier A transmission doubles by half and has 2 extra years of warranty compared to supplier B transmission. This means that supplier A transmission is dominating in this factor and it will be risky for supplier B transmission as the part price will doubles after the warranty period has ended.

As for the serviceability, the transmission oil price for transmission B is cheaper by 60% comparing to A.

In this case, the period of warranty plays a bigger role it will cause a bigger cost damage compared to the serviceability factor. This is measured based on the riskiness level where a vehicle parts can become faulty at any period while the servicing of car is only required at either 60000km or 120000km. Therefore, supplier A's transmission has a better after market value compared to supplier B's transmission.

#### 1.4 Recommendations

All in all, I would suggest supplier A transmission due to its good climb-ability, better response, a good after market value and also better fuel consumption. Since the target markets are fresh graduates and young executives, cost would be a priority in this case, and it is better for them to choose a vehicle with longer warranty period. This is because the part price will double up when the warranty is over.

Also, they are more of an active user where the vehicle will be used more frequently. In this case, better fuel consumption will be an important factor for them to choose A.

## 2.0 Assignment Task 2

a)

### 2.1 Data Tabulation

Table 3.0 Tabulation of Data

Plane	Mass (m), kg	Radius (r), m	$F_c / w^2$ (m*r), kg.m	Distance from plane 2 (l), m	Couple / $w^2$ (m.r.l), kg.m <sup>2</sup>
1	400	0.3	120	-0.45	-54
2	m <sub>2</sub>	0.3	0.3 m <sub>2</sub>	0	0
3	m <sub>3</sub>	0.3	0.3 m <sub>3</sub>	0.75	0.225 m <sub>3</sub>
4	400	0.3	120	1.35	162

### Examples of calculations

$F_c$

$$F_c = m \times r$$

$$= 400\text{kg} \times 0.3\text{m}$$

$$= 120 \text{ kg.m}$$

Couple

$$\text{Couple} = m \times r \times l$$

$$= 400\text{kg} \times 0.3\text{m} \times -0.45\text{m}$$

$$= -54 \text{ kg.m}^2$$

## 2.2 Solid Works Drawings

### 2.2.1 Primary Crank Positions

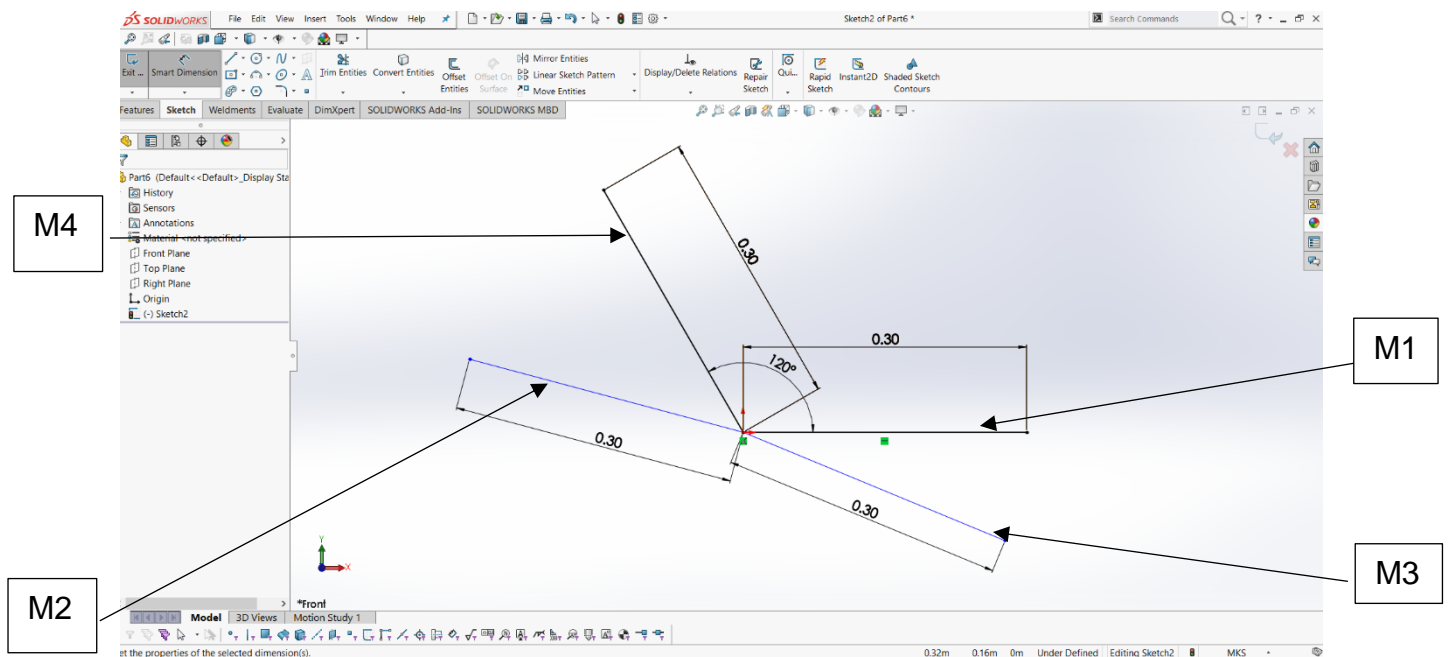


Figure 5.0 SolidWorks sketch of primary crank positions

### 2.2.2 Primary Couple Polygon

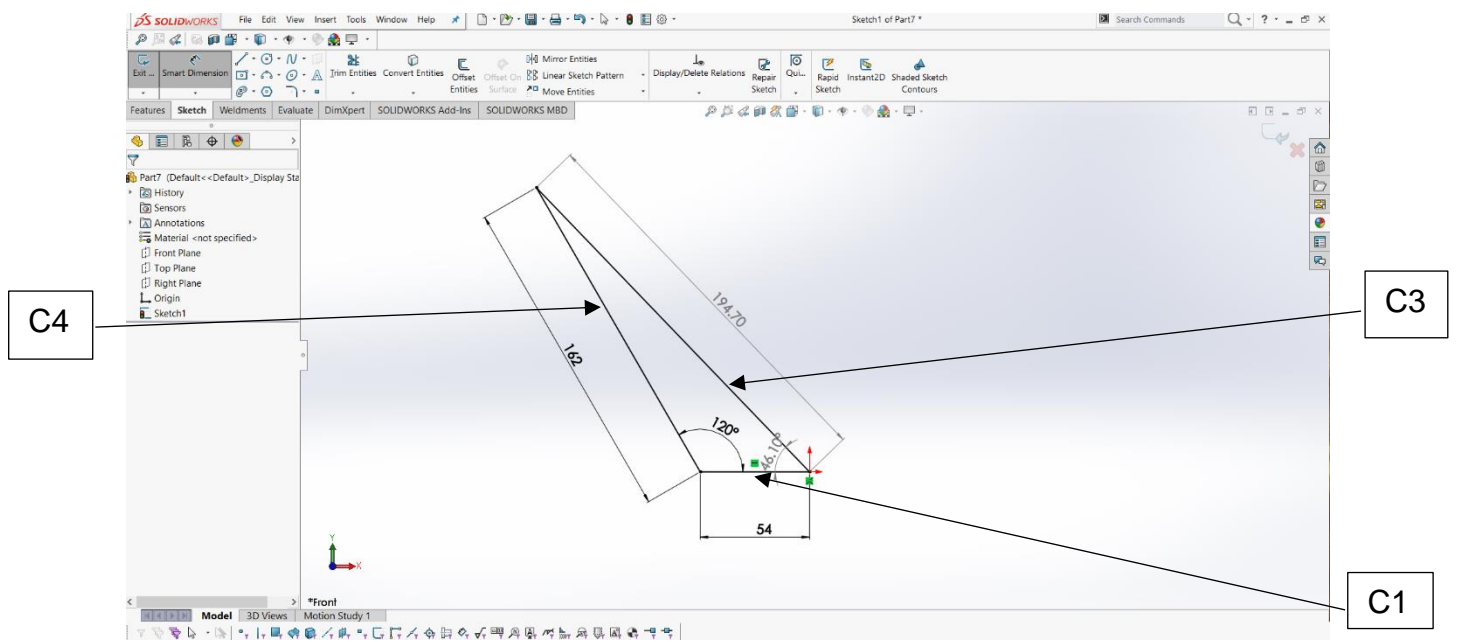


Figure 6.0 SolidWorks sketch of primary couple polygons

## 2.2.3 Primary Force Polygon

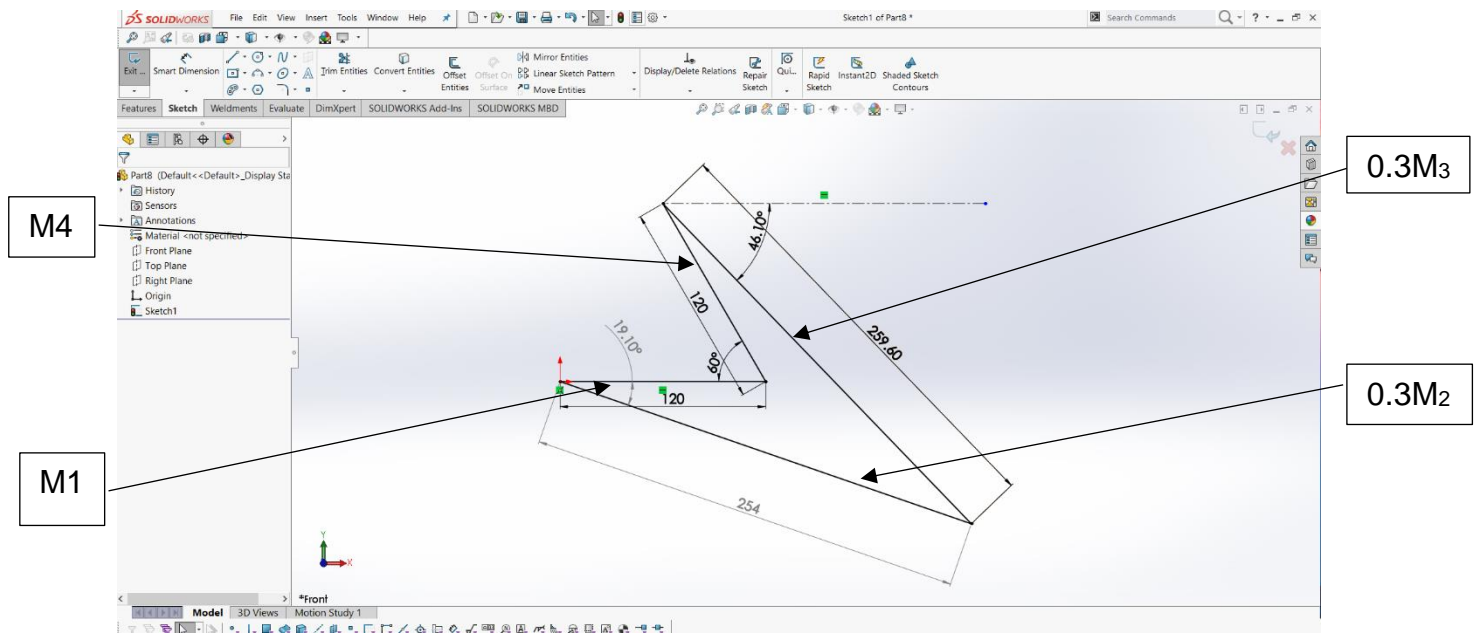


Figure 7.0 SolidWorks sketch of primary force polygon

## 2.2.4 Secondary Crank Positions

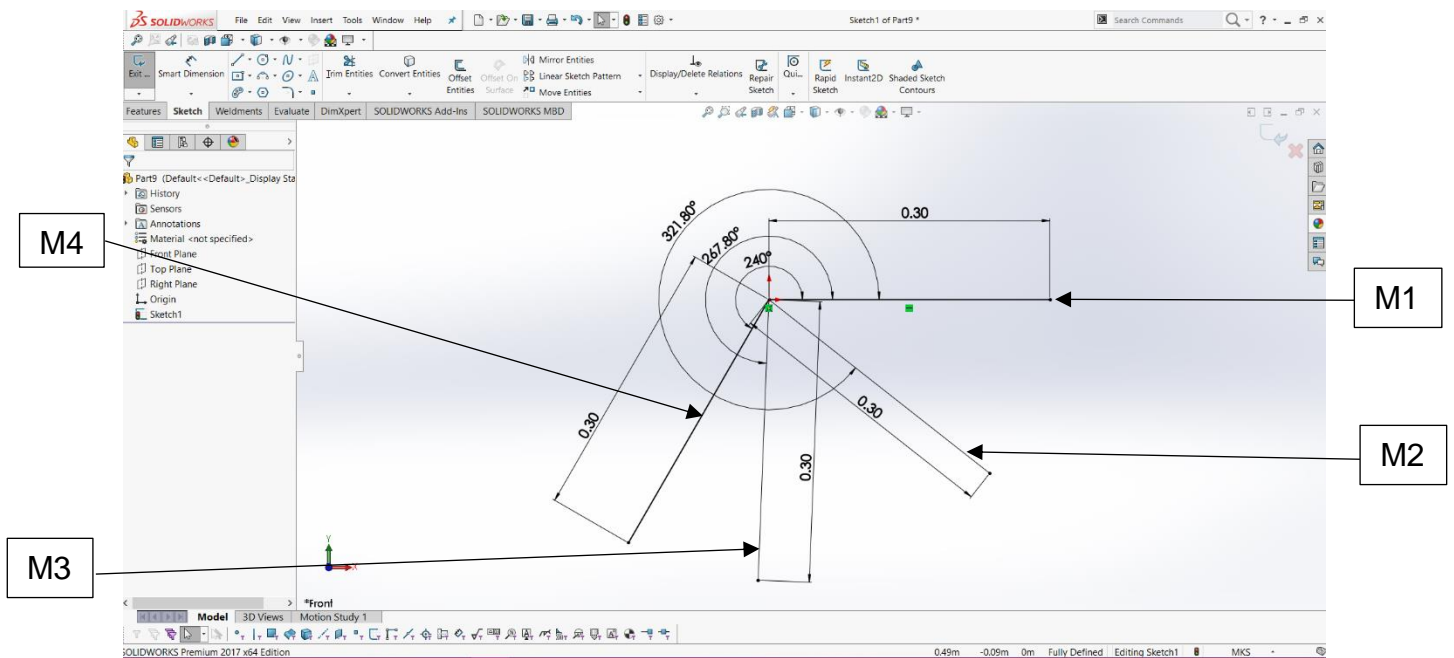


Figure 8.0 SolidWorks sketch of secondary crank positions

## 2.2.5 Secondary Force Polygon

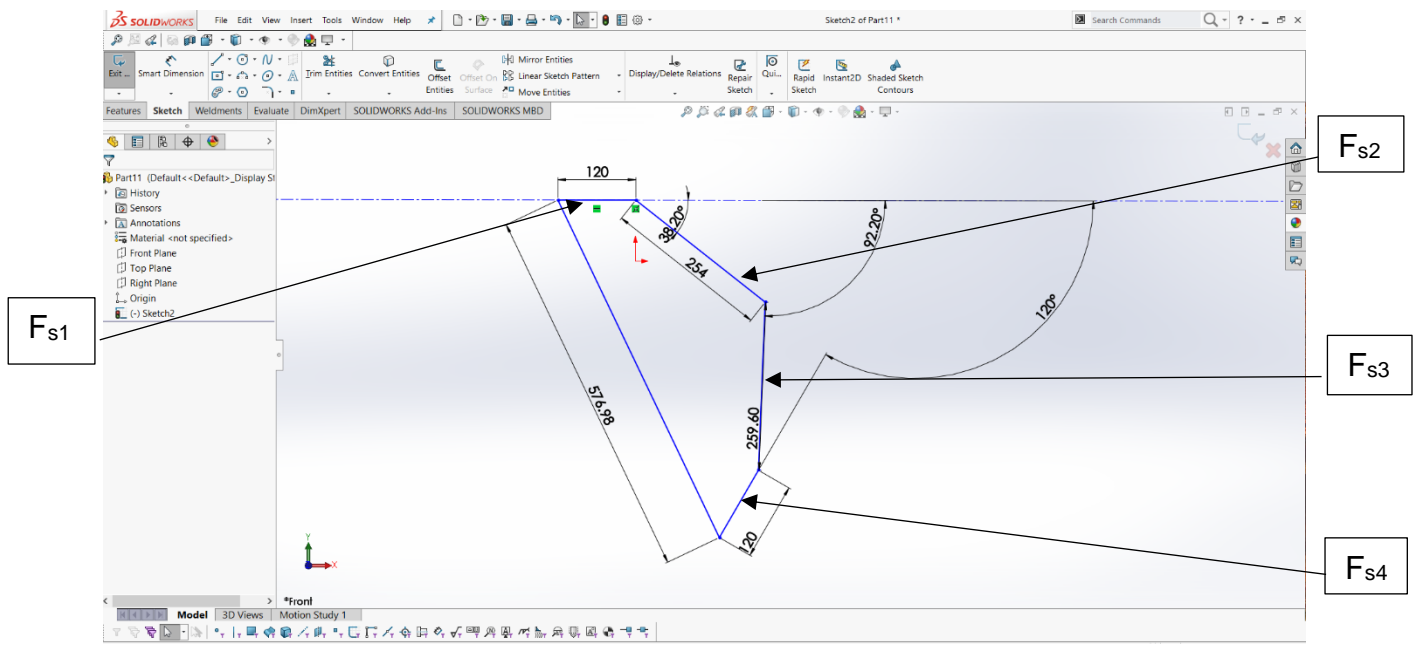


Figure 9.0 SolidWorks sketch of secondary force polygon

### Measurement of Secondary Unbalanced Force

$$F_{s(\max)} = 576.98 \text{ m}$$

b)

$$\text{The mass of } m_2 = \frac{254}{0.3}$$

$$= 846.67 \text{ kg}$$

$$\text{The mass of } m_3 = \frac{194.7}{0.225}$$

$$= 865.33 \text{ kg}$$

Table 4.0 Tabulation of Datas

Range of Engine Speed, (rpm)	$\omega$ , rad/s	Maximum Secondary Unbalanced Forces			
		Mass of cranks, kg			
		M1= 400	M2 = 846.67	M3=865.33	M3=400
0	0	0	0	0	0
100	10.472	3289.868	6963.582	7117.054	3289.868
200	20.944	13159.473	27854.327	28468.216	13159.473
300	31.416	29608.813	62672.235	64053.486	29608.813
400	41.888	52637.890	111417.306	113872.864	52637.890
500	52.360	82246.703	174089.541	177926.350	82246.703
600	62.832	118435.253	250688.939	256213.943	118435.253
700	73.304	161203.539	341215.500	348735.645	161203.539
800	83.776	210551.561	445669.224	455491.455	210551.561
900	94.278	266479.319	564050.112	576481.372	266479.319
1000	104.720	328986.813	696358.163	711705.398	328986.813

### Examples of calculations

Rpm =  $\omega$

$$\omega = \frac{100rpm}{1sec} \times \frac{1min}{60sec} \times \frac{2 \times \pi}{1}$$

$$= 10.472 \text{ rad/s}$$

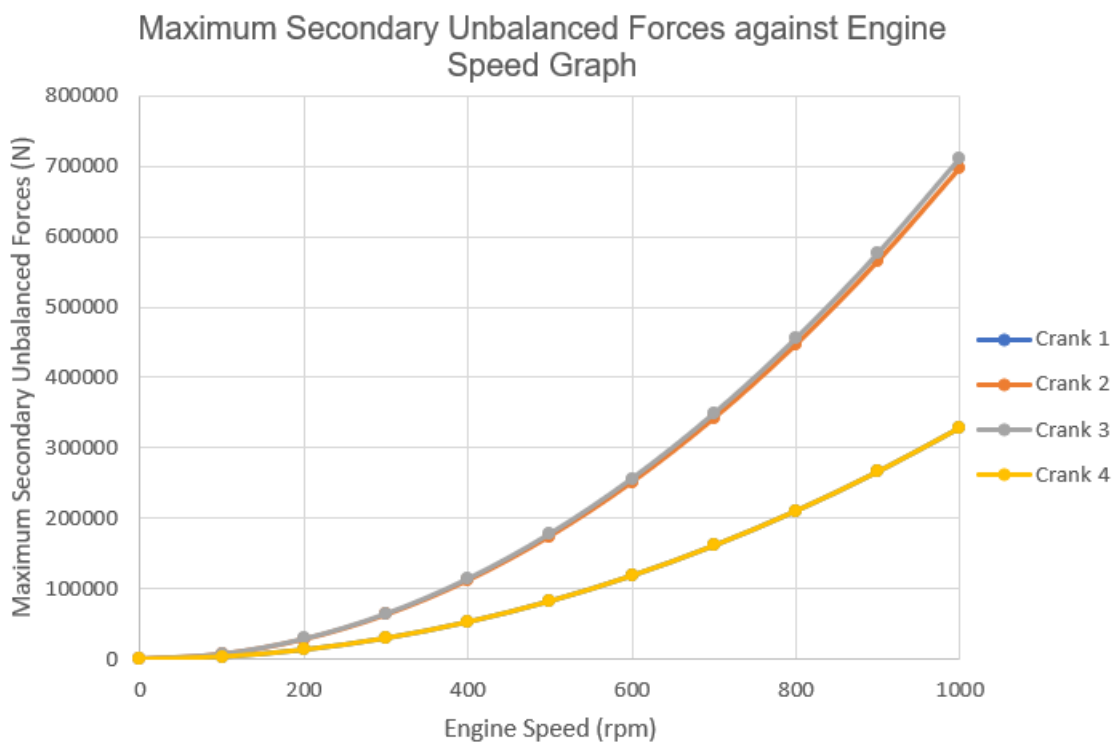


$F_{s(max)}$

Given crank radius,  $n=4$  , mass=400kg,  $\omega=10.472\text{rad/s}$ ,  $r=0.3\text{m}$

$$F_{s(max)} = (400\text{kg}) \times (10.472\text{rad/s})^2 \times \frac{0.3\text{m}}{4}$$
$$= 3289.868 \text{ N}$$

### 2.3 Graph of Maximum secondary unbalanced force against engine speed



#### Analysing

The graph shows that the maximum secondary unbalanced force is increasing proportionally with the engine speed. Crank 1 and crank 4 has the lowest maximum secondary unbalanced force but both have the same values since both of their masses are the same (400kg). Hence, the graph lines for both crank 1 and 4 overlap one another. Crank 3 has the highest maximum secondary unbalanced forces followed by crank 2, crank 1 and crank 4.

c)

Table 5.0 Tabulation of Data

Range of Engine Speed, (rpm)	$\omega$ , rad/s	Maximum Secondary Unbalanced Forces			
		Mass of cranks, kg			
		M1= 400	M2 = 846.67	M3=865.33	M3=400
1	31.416	118435.253	250688.939	256213.943	118435.253
2	31.416	59217.626	125344.470	128106.972	59217.626
3	31.416	39478.418	83562.980	85404.648	39478.418
4	31.416	29608.813	62672.235	64053.486	29608.813
5	31.416	23687.051	50137.788	51242.789	23687.051
6	31.416	19739.209	41781.490	42702.324	19739.209
7	31.416	16919.322	35812.706	36601.992	16919.322
8	31.416	14804.407	31336.117	32026.743	14804.407
9	31.416	13159.473	27854.327	28468.216	13159.473
10	31.416	11843.525	25068.894	25621.394	11843.525

### Examples of calculations

Rpm =  $\omega$

$$\omega = \frac{300 \text{ rpm}}{1 \text{ sec}} \times \frac{1 \text{ min}}{60 \text{ sec}} \times \frac{2 \times \pi}{1}$$

$$= 31.416 \text{ rad/s}$$

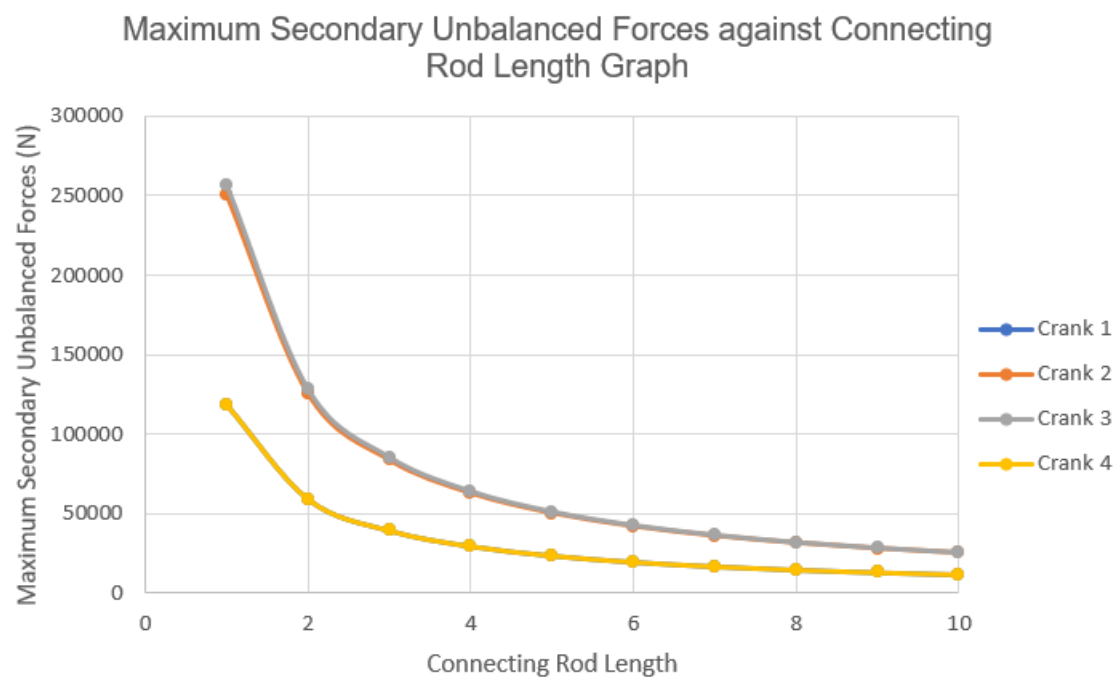
$F_{s(max)}$

Given crank radius,  $n=1$ , mass=400kg,  $\omega=31.416\text{rad/s}$ ,  $r=0.3\text{m}$

$$F_{s(max)} = (400\text{kg}) \times (31.416\text{rad/s})^2 \times \frac{0.3\text{m}}{1}$$

$$= 118435.807 \text{ N}$$

## 2.4 Graph of Maximum secondary unbalanced force against connecting rod length



### Analysing

The graph shows that the maximum secondary unbalanced force is decreasing proportionally with the length of connecting rod. Crank 1 and crank 4 graph lines overlap one another again due to the same mass of 400 kg. Both have a smaller gradient comparing to crank 2 and crank 3. Crank 3 has a higher gradient comparing to crank 2 due to its highest mass but both have the same decreasing trend.

d)

## 2.5 Conclusion

As a conclusion, the maximum secondary unbalanced force (N) will increase proportionally with the speed of the engine (rpm). On the other hand, the maximum secondary unbalanced force will decrease proportionally with the length of connecting rod.

## 3.0 References

1. Yamsani, A. (2014). Gradeability for Automobiles. *IOSR Journal of Mechanical and Civil Engineering*, 11(2), pp.35-41.
2. Nam, K., Hori, Y. and Lee, C. (2015). Wheel Slip Control for Improving Traction-Ability and Energy Efficiency of a Personal Electric Vehicle. *Energies*, 8(7), pp.6820-6840.
3. Hooftman, N., Oliveira, L., Messagie, M., Coosemans, T. and Van Mierlo, J. (2016). Environmental Analysis of Petrol, Diesel and Electric Passenger Cars in a Belgian Urban Setting. *Energies*, 9(2), p.84.
4. European Commission (2005). *Clean cars: Commission proposes to reduce emissions*. [online] Available at: [http://europa.eu/rapid/press-release\\_IP-05-1660\\_en.htm](http://europa.eu/rapid/press-release_IP-05-1660_en.htm) [Accessed 15 Jun. 2019].